

# ECC100 Series



- -40 °C to +75 °C Operation
- 100 W Baseplate Cooled
- High Efficiency Resonant Topology
- Screw Terminals Available
- 5V Standby Output
- Remote On/Off & Power OK Signal
- 3 Year Warranty

The ECC100 is a conduction cooled single output AC-DC power supply. It is designed for use in harsh environments where wide temperature variation and sealed enclosure installation is common place. Featuring highly efficient resonant mode topology, whilst maintaining its cost effectiveness, the ECC100 also provides remote sense, remote on/off, a combined AC & DC fail signal which coupled with its own standby rail ensures that control and status reporting is easily achievable.

Comprehensive overload, short circuit, over voltage and over temperature are built into the ECC100 as standard. An optional surge filter provides further protection from incoming AC surges to level 4 of EN61000-4-5.



#### Models and Ratings

Output Power	Output Voltage V1	Max Output Current V1	Standby Supply V2	Model Number
100 W	12.0 VDC	8.1 A	5.0 V/0.5 A	ECC100US12
100 W	15.0 VDC	6.5 A	5.0 V/0.5 A	ECC100US15
100 W	24.0 VDC	4.1 A	5.0 V/0.5 A	ECC100US24
100 W	28.0 VDC	3.5 A	5.0 V/0.5 A	ECC100US28
100 W	48.0 VDC	2.0 A	5.0 V/0.5 A	ECC100US48

#### Notes:

For optional surge filter add suffix '-F' to model number, e.g. ECC100US12-F.
Add suffix -S for screw terminals, consult sales for restrictions and availability.

#### **Input Characteristics**

Characteristic	Minimum	Typical	Maximum	Units	Notes & Conditions
Input Voltage - Operating	85	115/230	264	VAC	Derate output power < 90 VAC. See fig. 1. Power OK signal cannot be used <90 VAC.
Input Frequency	47	50/60	400	Hz	Agency approval 47-63 Hz
Power Factor		>0.5			230 VAC, 100% load EN61000-3-2 class A compliant
Input Current - No Load		0.07/0.09		A	115/230 VAC
Input Current - Full Load		1.5/0.9		A	115/230 VAC
Inrush Current			40	A	230 VAC cold start, 25 °C
Fauth Leakage Current		110/190	300	μA	115/230 VAC/50 Hz (Typ.), 264 VAC/60 Hz (Max.)
Earth Leakage Current		0.5/1.2		mA	115/230 VAC/400 Hz
Input Protection	T5.0A/250 V inte	ernal fuse in both li	ne and neutral	•	•

#### **Output Characteristics**

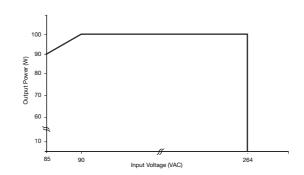
Characteristic	Minimum	Typical	Maximum	Units	Notes & Conditions
Output Voltage - V1	12		48	VDC	See Models and Ratings table
Initial Set Accuracy			±1 (V1) & ±3(V2)	%	50% load, 115/230 VAC
Output Voltage Adjustment	±5			%	V1 only via potentiometer. See mech. details (P13).
Minimum Load	0			A	
Start Up Delay		1.0		S	230 VAC full load (see fig.2)*
Hold Up Time	16	20		ms	115 VAC full load (see fig.3 & 4)
Drift			±0.2	%	After 20 min warm up
Line Regulation			±0.5	%	90-264 VAC
Load Regulation			±1 <sup>(V1)</sup> , ±5 <sup>(V2)</sup>	%	0-100% load
Transient Response - V1			4	%	Recovery within 1% in less than 500 µs for a 50-75% and 75-50% load step
Over/Undershoot - V1		5		%	See fig.5
Ripple & Noise			1 <sup>(V1)</sup> & 2 <sup>(V2)</sup>	% pk-pk	20 MHz bandwidth (see fig.6 & 7)
Overvoltage Protection	115		140	%	Vnom DC. Output 1 only, recycle input to reset
Overload Protection	110		150	% I nom	Output 1 only, auto reset (see fig.8)
Short Circuit Protection					Continuous, trip & restart (hiccup mode) all outputs
Temperature Coefficient			0.05	%/°C	
Overtemperature Protection		110		°C	Main transformer sensor shutdown

\* At low temperature and low line voltage, start up time will increase.

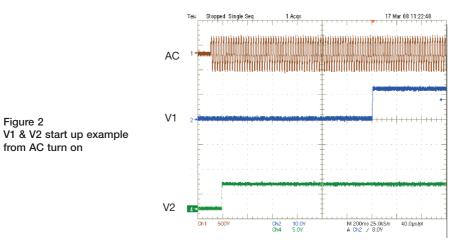


#### Input Voltage Derating

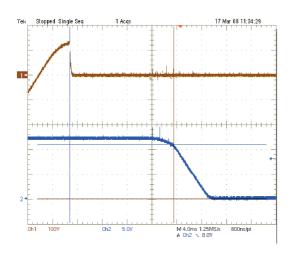
Figure. 1

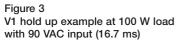


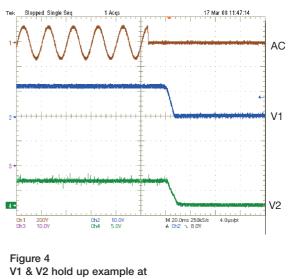
### Start Up Delay From AC Turn On

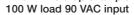


#### Hold Up Time From Loss of AC











#### **Output Overshoot**

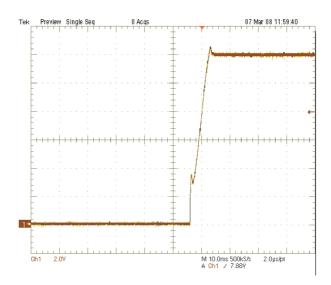


Figure 5 Typical Output Overshoot (ECC100US12 shown)

#### **Output Ripple & Noise**

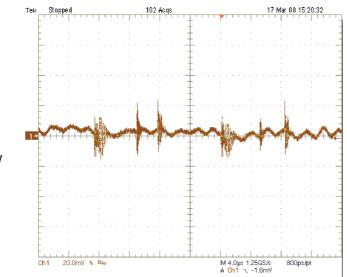


Figure 6 V1 ECC100 (full load) 27 mV pk-pk ripple. 20 MHz BW



#### Output Ripple & Noise cont.

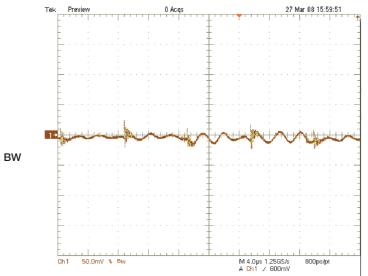


Figure 7 V1 ECC100US12 (full load) 39 mV pk-pk ripple. 20 MHz BW

#### **Output Overload Characteristic**

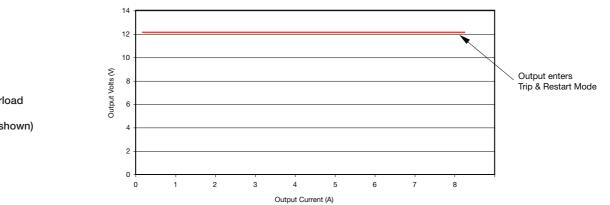


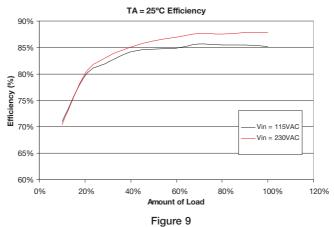
Figure 8 Typical V1 Overload Characteristic (ECC100US12 shown)



#### **General Specifications**

Characteristic	Minimum	Typical	Maximum	Units	Notes & Conditions
Efficiency		88		%	Full load (see fig.9 & 10)
Isolation: Input to Output	4000			VAC	
Input to Ground	1500			VAC	
Output to Ground	500			VAC	
Switching Frequency		70		kHz	
Power Density			3.9	W/in <sup>3</sup>	
Mean Time Between Failure		236		kHrs	MIL-HDBK-217F, Notice 2 +25 °C GB
Weight			0.7 (320)	lb (g)	

## Efficiency Versus Load



ECC100US12 at 115 & 230 VAC

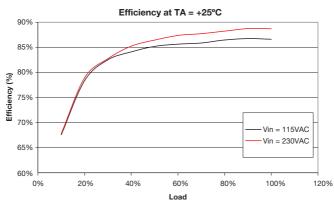


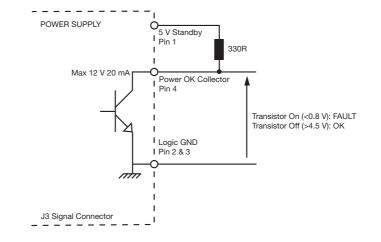
Figure 10 ECC100US24 at 115 & 230 VAC

Characteristic	Notes & Conditions
Signals & Control	
Remote Sense	Compensates for 0.5 V total voltage drop
Power OK (combined AC OK & DC OK)	Open collector referenced to logic ground & output 0V, transistor normally off when AC is good (see fig.11 - 15) AC OK: Provides ≥ 3 ms warning of loss of output from AC failure
Remote On/Off (Inhibit/Enable)	Uncommited isolated optocoupler diode, powered diode inhibits the supply (see fig.16-21)
Standby Supply V3	5 V/0.5 A supply, always present when AC supplied, referenced to logic ground and output 0V



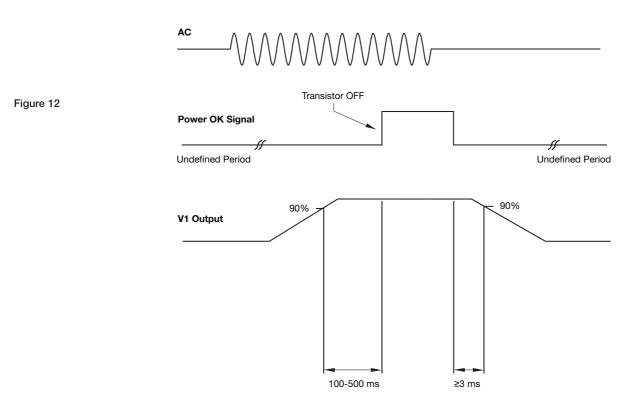
#### Signals

#### Power OK



## Figure 11

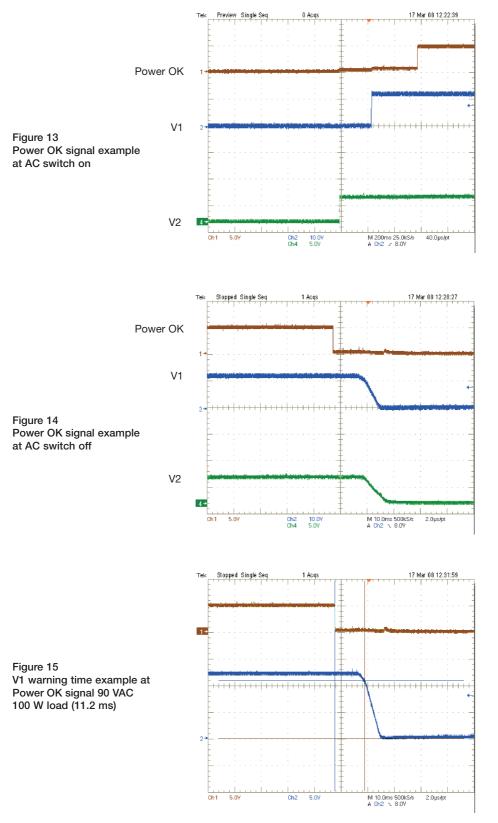
#### Power OK - Timing Diagram





## Signals (cont'd)

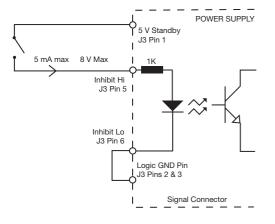
#### Power OK





#### Signals (cont'd)

#### Remote On/Off (Inhibit/Enable)



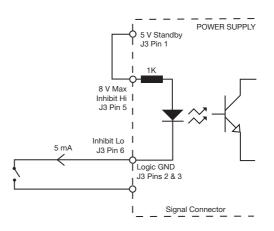
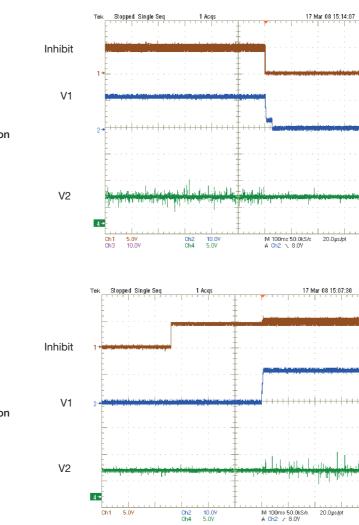
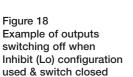


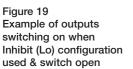
Figure 17

Inhibit (Lo)





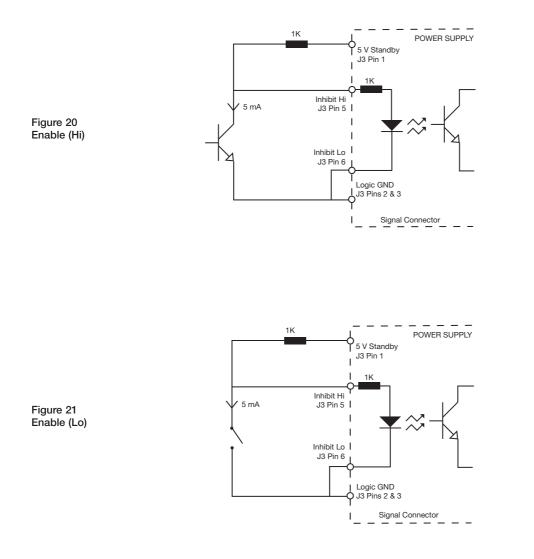






#### Signals (cont'd)

### Remote On/Off (Inhibit/Enable)





#### Environmental

Characteristic	Minimum	Typical	Maximum	Units	Notes & Conditions
Operating Temperature	-40		+75	°C	Baseplate must not exceed 85°C. See thermal considerations.
Warm Up Time		20		Minutes	
Storage Temperature	-40		+85	°C	
Cooling					Baseplate cooled
Humidity	5		95	%RH	Non-condensing
Operating Altitude			3000	m	
Shock					3 x 30 g/11 ms shocks in both +ve & -ve directions along the 3 orthogonal axis, total 18 shocks.
Vibration					Triple axis 5-500 Hz at 2 g x 10 sweeps

#### Electromagnetic Compatibility - Immunity

Phenomenon	Standard	Test Level	Criteria	Notes & Conditions
Low Voltage PSU EMC	EN61204-3	High severity level	as below	
Harmonic Current	EN61000-3-2	Class A		
Radiated	EN61000-4-3	3	А	
EFT	EN61000-4-4	3	А	
Surges	EN61000-4-5	Installation class 3	А	
Surges	LIN01000-4-5	Installation class 4	А	With option -F
Conducted	EN61000-4-6	3	A	
		Dip: 30% 10 ms	А	
Dips and Interruptions	EN61000-4-11	Dip: 60% 100 ms	В	
		Dip: 100% 5000 ms	В	

#### **Electromagnetic Compatibility - Emissions**

Phenomenon	Standard	Test Level	Criteria	Notes & Conditions
Conducted	EN55022	Class B		
Radiated	EN55022	Class A		
Voltage Fluctuations	EN61000-3-3			

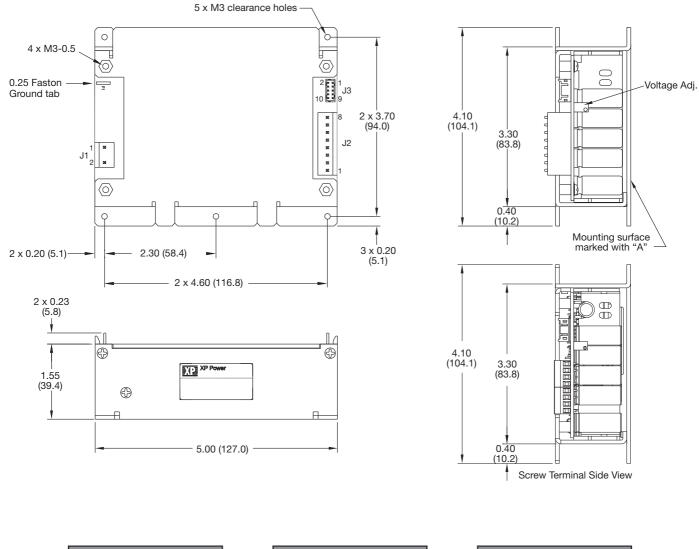
#### Safety Agency Approvals

Safety Agency	Safety Standard	Category
CB Report	UL File #E139109-A42-CB-1, IEC60950-1 (2005) Second Edition	Information Technology
UL	UL File #E139109-A42-UL, UL60950-1, 2nd Edition, 2007-03-27, CSA C22.2 No 60950-1-07 2nd Edition 2007-03	Information Technology
TUV	TUV Certificate B 09 12 57396 067, EN60950-1/A11:2009	Information Technology
CE	LVD	

Equipment Protection Class	Safety Standard	Notes & Conditions
Class I	IEC60950-1:2005 Ed 2	See safety agency conditions of acceptibility for details



#### Mechanical Details - ECC100USxx



C	Output Connector J2				
N	Molex PN 09-65-2088				
Pin	Single Output				
1	+V1				
2	+V1				
3	+V1				
4	+V1				
5	RTN				
6	RTN				
7	RTN				
8	RTN				

J2 mates with Molex housing PN 09-50-1081 and both with Molex series 5194 crimp terminals.

Input Connector J1				
Molex PN 09-65-2038				
1	Line			
2	Neutral			
J1 mates PN 09-50	with Molex housing 0-1031.			

	Signal Connector J3 Molex PN B10B-PHDSS	
1	+5 V Standby	
2	Logic GND	
3	Logic GND	
4	Power OK	
5	Inhibit Hi	
6	Inhibit Lo	
7	+Sense	
8	-Sense	
9	+Vout	
10	-Vout	

J3 mates with JST housing PN PHDR-10VS and with JST SPHD-001T-P0.5 crimp terminals.

#### Notes

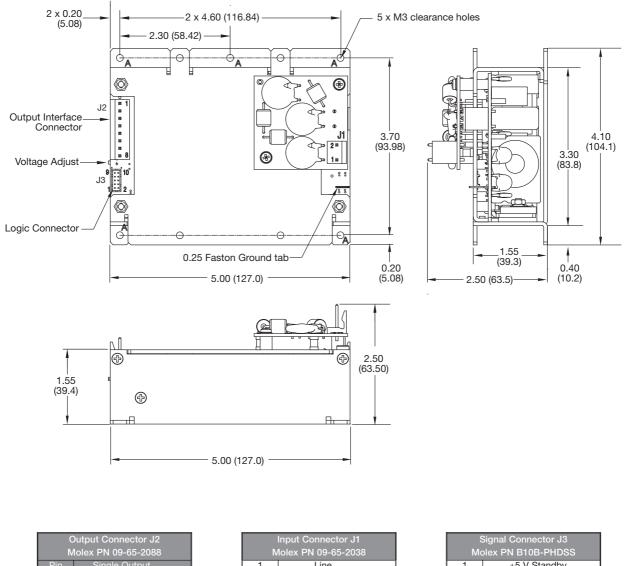
1. All dimensions in inches (mm).

2. Tolerance  $.xx = \pm 0.02 (0.50)$ ;  $.xxx = \pm 0.01 (0.25)$ 

3. Weight 1.2 lbs (550g)



#### Mechanical Details - ECC100USxx-F



Molex PN 09-65-2088		
Pin	Single Output	
1	+V1	
2	+V1	
3	+V1	
4	+V1	
5	RTN	
6	RTN	
7	RTN	
8	RTN	
J2 mates with Molex housing PN		

09-50-1081 and both with Molex series 5194 crimp terminals.

Input Connector J1 Molex PN 09-65-2038		
1	Line	
2	Neutral	
I1 mates with Molex housing		

IU PN 09-50-1031.

Signal Connector J3 Molex PN B10B-PHDSS	
1	+5 V Standby
2	Logic GND
3	Logic GND
4	Power OK
5	Inhibit Hi
6	Inhibit Lo
7	+Sense
8	-Sense
9	+Vout
10	-Vout

J3 mates with JST housing PN PHDR-10VS and with JST SPHD-001T-P0.5 crimp terminals.

#### Notes

- 1. All dimensions in inches (mm).
- 2. Tolerance  $.xx = \pm 0.02$  (0.50);  $.xxx = \pm 0.01$  (0.25)

3. Weight 1.2 lbs (550g)



#### Thermal Considerations - Baseplate Cooling

The use of power supplies in harsh or remote environments brings with it many fundamental design issues that must be fully understood if long-term reliability is to be attained.

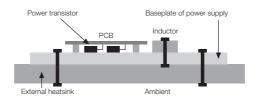
Under these conditions, it is generally accepted that electronic systems have to be sealed against the elements. This makes the removal of unwanted heat particularly difficult. The use of forced-air cooling is undesirable as it increases system size, adds the maintenance issues of cleaning or replacing filters, and the fan being prone to wear out, particularly in tough environments.

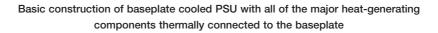
The extremes of ambient temperature encountered in remote sites can range from -40 °C to over+40 °C. It is common for the temperature within the enclosure to rise some 15 to 20 °C above the external temperature. The positioning of the power supply within the enclosure can help minimize the ambient temperature in which it operates and this can have a dramatic effect on system reliability.

System enclosures are typically sealed to IP65, IP66 or NEMA 4 standards to prevent ingress of dust or water. Removal of heat from other electronic equipment and power supplies in a situation with negligible airflow is the challenge. From the power system perspective, the most effective solution is to remove the heat using a heatsink that is external to the enclosure. However, most standard power supplies cannot provide an adequate thermal path between the heat-dissipating components within the unit and the external environment.

Fundamentally, the successful design of a power supply for use within sealed enclosures relies on creating a path with low thermal resistance through which conducted heat can be passed from heat- generating components to the outside world.

The components that generate the most heat in a power supply are distributed throughout the design, from input to output. They include the power FET used in an active PFC circuit, the PFC inductor, power transformers, rectifiers, and power switches. Heat can be removed from these components by thermally connecting them to the base-plate that in turn can be affixed to a heatsink. As mentioned earlier, the heatsink is then located outside of the enclosure.





#### Dissipating the Heat: Heatsink Calculations

Three basic mechanisms contribute to heat dissipation: conduction, radiation and convection. All mechanisms are active to some degree but once heat is transferred from the baseplate to the heatsink by conduction, free convection is the dominant one.

Effective conduction between the baseplate and heatsink demands flat surfaces in order to achieve low thermal resistance. Heat transfer can be maximized by the use of a thermal compound that fills any irregularities on the surfaces. System designers should aim to keep thermal resistance between baseplate and heatsink to below 0.1 °C/W. This is the performance offered by most commonly used thermal compounds when applied in accordance with manufacturers' instructions.

Radiation accounts for less than 10% of heat dissipation and precise calculations are complex. In any case, it is good practice to consider this 10% to be a safety margin.



The following example shows how to calculate the heatsink required for an ECC100US12 with 230 VAC input and an output load of 90 W operating in a 40 °C outside ambient temperature.

1. Calculate the power dissipated as waste heat from the power supply. The efficiency (see fig. 9 & 10) and worst case load figures are used to determine this using the formula:

Waste heat =  $\left\{\frac{1 - \text{Eff\%}}{\text{Eff\%}}\right\} x \text{ Pout}$  =  $\left\{\frac{1 - 0.87}{0.87}\right\} x 90 \text{ W}$  = 13.5 W

2. Estimate the impedance of the thermal interface between the power supply baseplate and the heatsink. This is typically 0.1°C/W when using a thermal compound.

3. Calculate the maximum allowable temperature rise on the baseplate. The allowable temperature rise is simply:

## $T_B$ – $T_A$ where $T_A$ is the maximum ambient temperature outside of the cabinet and $T_B$ is the maximum allowable baseplate temperature.

4. The required heatsink is defined by its thermal impedance using the formula:

$$\theta H = \frac{T_B - T_A}{Waste Power} - 0.1 = \frac{85 \text{ °C} - 40 \text{ °C}}{13.5 \text{ W}} - 0.1 = 3.23 \text{ °C/W}$$

5. The final choice is then based on the best physical design of heatsink for the application that can deliver the required thermal impedance. The system's construction will determine the maximum available area for contact with the baseplate of the power supply and the available space outside of the enclosure will then determine the size, number and arrangement of cooling fins on the heatsink to meet the dissipation requirement.